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- The API Standard 526 lists standard characteristics for relief devices for a given orifice size:
 - Inlet / Outlet Diameters
 - Flange Ratings
 - Temperature / Pressure Limits
 - Backpressure Limits
 - Dimensions
- Relief Device Installation Requirements dictate:
 - Inlet pressure loss requirements
 - Outlet pressure loss requirements

Table 4—Spring-loaded Pressure-relief Valves "E" Orifice (Effective Orifice Area = 0.196 in.2)

Materials ^b	Valve Size	Fla	ME nge ass		Maximum I	inlet Flange (p:	Li	Pressure mit ^a	Dime	r-to-Face			
					Convention	nal and Bal	(psig)		(III.)				
Body/ Bonnet	Inlet by Orifice by Outlet	I N L E T	O T L E T	-450°F to -75°F	-75°F to -21°F	-20°F to 100°F	450°F	800 °F	1000 °F	Flange Rating Limit ^a	Bellows Rating Limit ^a	I N L E T	0 U T L E
										100 °F	100°F		'
				Te	mperature i	Range Inclu	sive –20°F	to 800°F					
Carbon Steel	1E2 1E2 1E2 1E2 1 ½E2 1 ½E2 1 ½E2	150 300 300 600 900 1500 2500	150 150 150 150 300 300 300			285 (285) 740 1480 2220 3705 6000	185 (285) 615 1235 1845 3080 6000	80 (285) 410 825 1235 2060 3430		285 285 285 285 (600) (600) 740	230 230 230 230 500 500	4 1/8 4 1/8 4 1/8 4 1/8 4 1/8 4 1/8 5 1/2	4 1/2 4 1/2 4 1/2 4 1/2 5 1/2 5 1/2 7
	1 122.0			Tr	mperature i	Range Indu	sive 801 °F	o 1000 °F					
Chrome Molybdenum Steel	1E2 1E2 1 ½E2 1 ½E2 1 ½E3	300 600 900 1500 2500	150 150 300 300 300					510 1015 1525 2540 4230	215 430 650 1080 1800	285 285 (600) (600) 740	230 230 500 500	4 1/8 4 1/8 4 1/8 4 1/8 5 1/2	4 1/2 4 1/2 5 1/2 5 1/2 7
				Te	mperature i	Range Inclu	sive -450 °F	to 1000°F					
Austenitic Stainless Steel	1E2 1E2 1E2 1E2 1½E2 1½E2 1½E2	150 300 300 600 900 1500 2500	150 150 150 150 300 300 300	275 (275) 720 1440 2160 3600 (4000)	275 (275) 720 1440 2160 3600 6000	275 (275) 720 1440 2160 3600 6000	180 (275) 495 975 1485 2480 4130	80 (275) 420 845 1265 2110 3520	20 (275) 350 700 1050 1750 2915	275 275 275 275 (600) (600) 720	230 230 230 230 500 500	4 1/8 4 1/8 4 1/8 4 1/8 4 1/8 4 1/8 5 1/2	4 1/2 4 1/2 4 1/2 4 1/2 5 1/2 5 1/2 7
	1 7220			Ti	emperature	Range Indu	sive -20 °F	to 900°F d					
Nickel/Copper Alloy ^d	1E2 1E2 ⁰ 1E2 1E2 1 ½E2	150 300 300 600 900	150 150 150 150 300			230 (230) 600 1200 1800	175 (230) 475 945 1420	80 (230) 460 915 1375	50 230 275 550 825	230 230 230 230 230 600	230 230 230 230 230 500	4 1/8 4 1/8 4 1/8 4 1/8 4 1/8	4 ½ 4 ½ 4 ½ 4 ½ 4 ½ 5 ½
				Te	mperature i			to 300 °F °					
Alloy 20 °	1E2 1E2° 1E2 1E2 1 ½E2 1 ½E2 1 ½E2	150 300 300 600 900 1500 2500	150 150 150 150 300 300 300			230 (230) 600 1200 1800 3000 5000	180 (180) 465 930 1395 2330 3880			230 230 230 230 600 600	230 230 230 230 500 500 500	4 1/8 4 1/8 4 1/8 4 1/8 4 1/8 4 1/8 5 1/2	4 ½ 4 ½ 4 ½ 4 ½ 5 ½ 5 ½ 7

Intel and outlet fange pressure limits correspond to the values in ASME B16.34 unless enclosed in parentheses. A value that is shown in parentheses is less than that provided in ASME B16.34. The outlet fange pressure values at other temperatures may only be interpolated using graphs from Annex B or from tables in ASME B16.34, if these values do not exceed the values in parentheses or the outlet fange values at 100 F above. Pressure changes within the temperature range above may not be inear. Believes outlet pressure limits are the design pressure of the believes at the outlet temperature of 100 Ft, and pressure values at other temperature may be determined from Annex C. User is causioned to mixe the outlet temperature for possible cryogenic applications and occide the appropriate materials.

Materials given are minimum requirements for the pressure and temperature ratings. Other suitable materials may be used, as required for the service involved.

Set pressure limited for low-oressure applications where a class 300 inlet flange is preferred over a class 150 flang

Materials limited to 900°F. Pressure ratings indicated in the 1000°F column are limited to 900°F.

Materials limited to 300° F. Pressure ratings indicated in the 450° F column are limited to 300° F.

 For many orifice sizes, there are multiple sizes depending on the required set pressure.

Size	D	E	F	G	Н	J	К	L	М	N	Р	Q	R	Т
1x2														
1½x2														
1½x3														
2x3														
3x4														
3x6														
4x6														
6x8														
6x10														
8x10														

- Inlet Pipe Area / Orifice Area less than ~ 3 tend to have difficulty meeting the 3% rule.
- Outlet Pipe Area / Orifice Area less than ~ 5.5 tend to have difficulty meeting the backpressure requirements (Hisao Izuchi, API Conference Meetings)



 For many orifice sizes, there are multiple valve configurations depending on the required set pressure.

Size	D	E	F	G	Н	J	K	L	М	N	Р	Q	R	Т
1x2														
1½x2														
1½x3														
2x3														
3x4														
3x6														
4x6														
6x8														
6x10														
8x10														

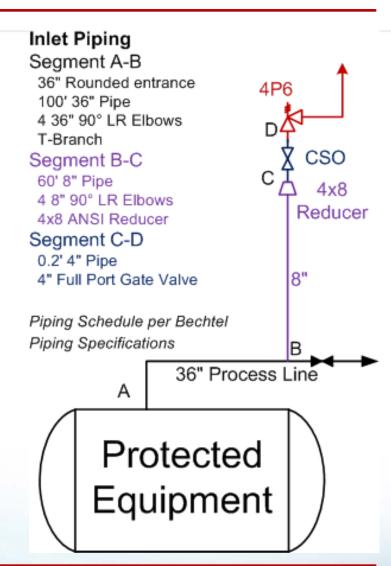
- $\frac{Orifice\ Area}{Inlet\ Pipe\ Area}$ < 3 tend to have difficulty meeting the 3% rule.
- Orifice Area outlet Pipe Area < 5.5 tend to have difficulty meeting the backpressure requirements (Hisao Izuchi, API Conference Meetings)

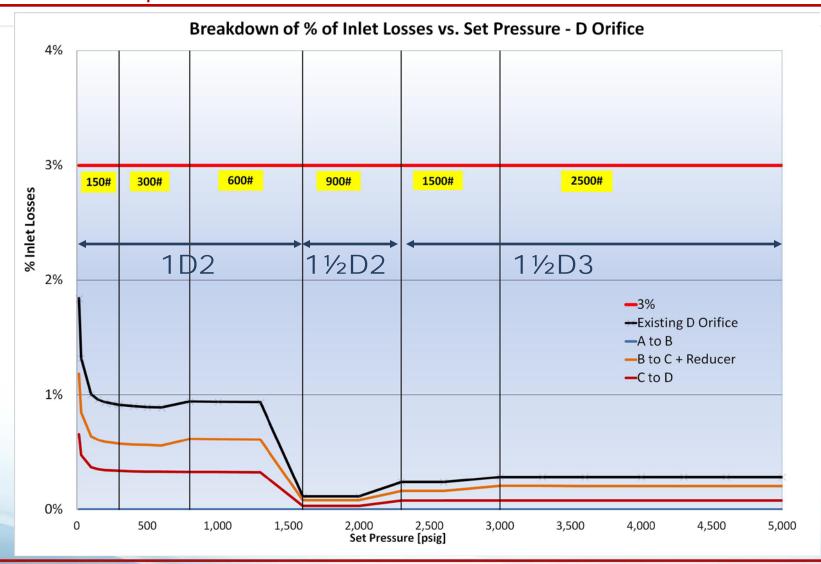
Orifice	Area	Size	M-IFR	OFR	CS P _{limit}	IP Sch	OP Sch	C - P _{Outlet}	B - P _{Outlet}	IPA / OA	OPA / OA
D	0.11	1x2	600	150	1,480	160	STD	285	230	4.7	30.5
	0.11	1½x2	1,500	300	3,705	XXS	STD	600	500	8.6	30.5
	0.11	1½x3	2,500	300	6,000	XXS	STD	740	500	8.6	67.2
Е	0.196	1x2	600	150	1,480	160	STD	285	230	2.7	17.1
	0.196	1½x2	1,500	300	3,705	XXS	STD	600	500	4.8	17.1
	0.196	1½x3	2,500	300	6,000	XXS	STD	740	500	4.8	37.7
F	0.307	1½x2	600	150	1,480	160	STD	285	230	4.6	10.9
	0.307	1½x3	2,500	300	5,000	XXS	STD	740	500	3.1	24.1
G	0.503	1½x3	900	300	2,220	160	STD	740	470	2.8	14.7
	0.503	2x3	2,500	300	3,705	XXS	STD	740	470	3.5	14.7
Н	0.785	1½x3	300	150	285	160	STD	285	230	1.8	9.4
	0.785	2x3	1,500	300	2,750	160	STD	740	415	2.8	9.4
J	1.287	2x3	300	150	285	STD	STD	285	230	2.6	5.7
	1.287	3x4	1,500	300	2,700	160	STD	600	230	4.2	9.9
K	1.838	3x4	600	150	1,480	XS	STD	285	200	3.6	6.9
	1.838	3x6	1,500	300	2,220	160	STD	600	200	2.9	15.7
L	2.853	3x4	300	150	285	STD	STD	285	100	2.6	4.5
	2.853	4x6	1,500	150	1,500	160	STD	285	170	3.3	10.1
М	3.6	4x6	900	150	1,100	XS	STD	285	160	3.2	8.0
N	4.34	4x6	900	150	1,000	XS	STD	285	160	2.6	6.7
Р	6.38	4x6	900	150	1,000	XS	STD	285	150	1.8	4.5
Q	11.05	6x8	600	150	600	XS	STD	115	115	2.4	4.5
R	16	6x8	300	150	100	STD	STD	60	60	1.8	3.1
	16	6x10	600	150	300	XS	STD	100	100	1.6	4.9
Т	26	8x10	300	150	300	STD	STD	100	100	1.9	3.0

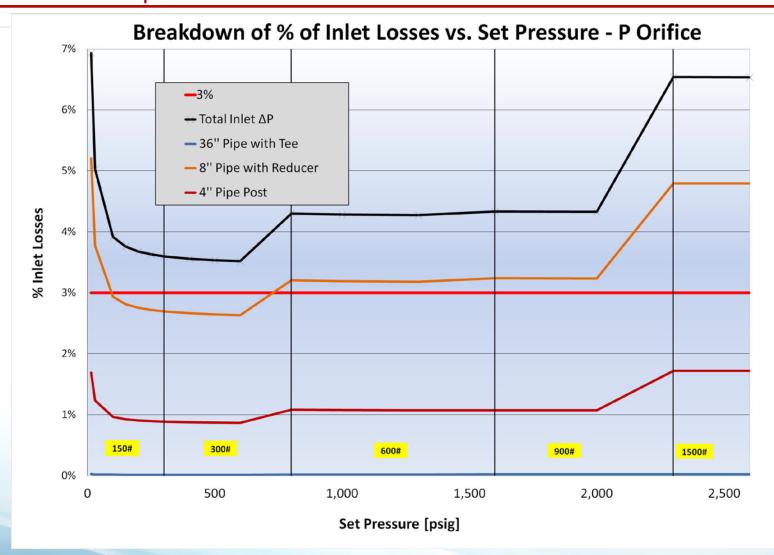
Set Pressure Limit (CS P_{LIMIT}) is for Carbon Steel @ 100 °F; M-IFR = Maximum Inlet Flange Rating, OFR = Outlet Flange Rating, IP Sch = Inlet Pipe Schedule, OP Sch = Outlet Pipe Schedule,

C - P_{Outlet} = Conventional Outlet Pressure limit, B - P_{Outlet} = Bellows Outlet, IPA / OA = Inlet Pipe Area / Orifice Area, OPA / OA = Outlet Pipe Area / Orifice Area.

- Methodology to identify valves with inlet installation problems:
 - Standard Common New Installation used (see figure)
 - Set Pressure varied from 15 psig to 5,000 psig (or the STD 526 limits)
 - Piping schedule varied to meet Bechtel Pipe Spec's based on the pressure limits @ 200°F
 - Relief device body sized varied to meet API STD 526 pressure limits @ 200°F
- Other Valve Sizes
 - A − B, always 36" pipe
 - B − C, 2x PSV Inlet Diameter







- The API Standard 526 Sizes that are difficult to install (over all set pressure ranges)
 - Purple Boxes are valves that have inlet installations concerns
 - Red Boxes are valves that have inlet and outlet installations concerns

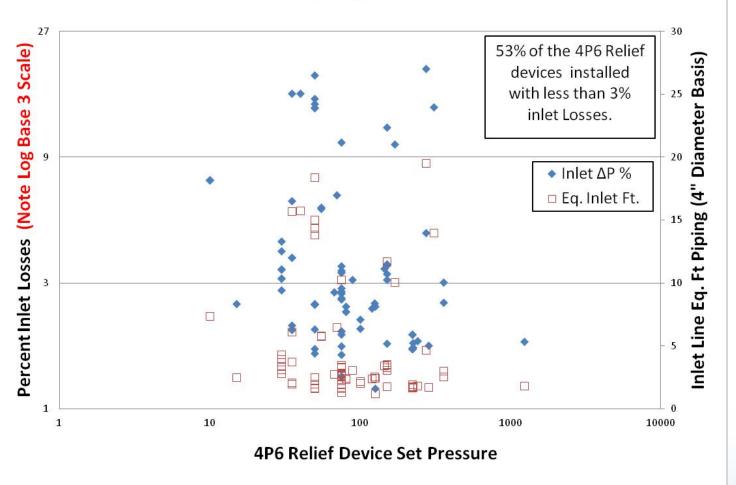
Size	D	E	F	G	Н	J	K	L	М	N	Р	Q	R	Т
1x2														
1½x2														
1½x3														
2x3														
3x4														
3x6														
4x6														
6x8														
6x10														
8x10														

 Outlet Pipe Area / Orifice Areas less than ~ 5.5 tend to have difficulty meeting the backpressure requirements (Hisao Izuchi, API Conference Meetings)



- What does this mean in the real world? Is it a problem?
 - For a large chemical plant in the USA:
 - 90 unique 4P6 relief devices
 - Set Pressure varied from 10 psig to 1,230 psig
 - Inlet piping equivalent feet varied from 4 ft to 116 ft
 - Inlet ΔP varied from 1.2% to 19.5%
 - Results
 - Inlet ΔP was less than 3% for 54% of the 4P6 relief devices (48/90)
 - Inlet ΔP was greater than 3% for 46% of the 4P6 relief devices (42/90)
- Previous standard common installation equivalent feet ~11





Q: How do we fix this real world problem?

A: Form a committee of course

- So API 526 formed a Task Force to investigate how:
 - To modify the relief device standard to ease meeting inlet piping installations requirements (e.g the API 3% rule)
 - To modify the relief device standard to ease meeting the outlet piping installation requirements
 - This information has come out of the API STD 526 Task Force and is being shared for comment
- A lot of work has been done to-date, a very brief summary of working solutions proposed are:
 - Option 1 Increase the body size for existing orifice sizes (e.g. a 6P8)
 - Option 2 Add an optimized size for each inlet valve diameter (e.g. 6Q'8, where Q' is \sim 8.82 in²; OA / IPA = 3.0 & OA / OPA = 5.7)
 - Option 3 Allow an option for manufacturers to provide valves of a customizable area (e.g. adjustable lift)
 - Option 4 Do nothing

Option 1 - Increase the body size for existing orifice sizes (e.g. a 6P8)

• Pros:

- Easy for industry to understand the change; does not introduce any new concepts
- Increased flexibility for new installations

Cons

- Does little to help mitigate the existing installation problems
- New options will drive up manufacturers' costs (and new relief device prices)
- If the standard eliminates or reduces the ability to use problem valves, will tend to drive up total installed costs for new installations
- Maintenance costs may increase due to the additional valve types to be stored, repaired, and spared



Option 2 - Add an optimized size for each inlet valve diameter (e.g. 6Q'8, where Q' is ~8.82 in²; OA / IPA = 3.0 & OA / OPA = 5.7)

Pros:

- Will allow the resolution of some inlet piping installation concerns (e.g. Inlet $\Delta P > 3\%$) to be resolved with piping changes
- Increased flexibility for new installations

Cons

- Introduces a new series of orifice letters and may cause confusion (as there
 are currently no letters between P and Q for the new Q')
- New options will drive up manufacturers' costs (and new relief device prices), but conceivably less than Option 1
- If the standard eliminates or reduces the ability to use problem valves, will tend to drive up total installed costs for new installations
- Maintenance costs may increase due to the additional valve types to be stored, repaired, and spared

• Option 3 - Allow an option for manufacturers to provide valves of a customizable area (e.g. adjustable lift).

• Pros:

- Will allow the most resolution of inlet piping installation concerns (e.g. Inlet $\Delta P > 3\%$) to be resolved without piping changes (of the 4 options)
- Increased flexibility for new installations
- Concept is already in use and has been accepted by the NB for UV stamping
- May reduce sparing and maintenance cost due to a consolidation of relief devices and internal parts

Cons

- Confusion, as this is a paradigm shift in the way that relief devices are designed and specified
- New options will drive up manufacturers' costs (and new relief device prices), but conceivably less than Option 1
- Whole new set of requirements will need to be codified and/or RAGAGEP'ed to deal with variable orifice areas in standard valve sizes



- Option 4 Do Nothing
- Pros:
 - Easiest to implement
 - No change-related PSV costs
- Cons
 - Few options other than piping modifications for retrofitting valves that do not meet installation requirements
 - Not actually a real solution

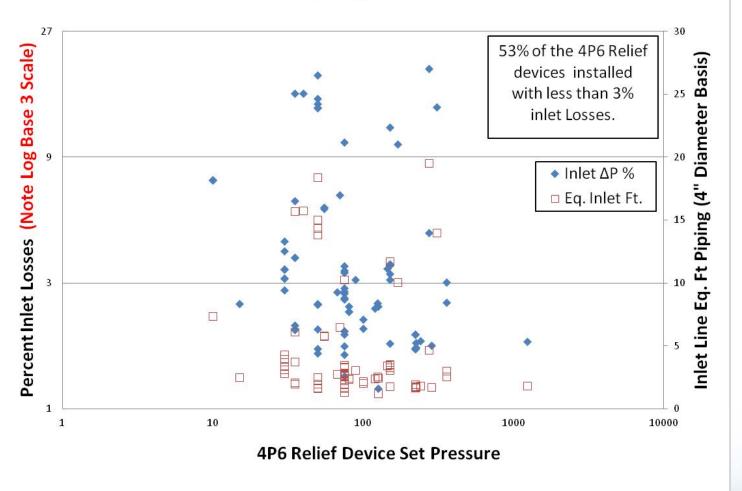


Comments?

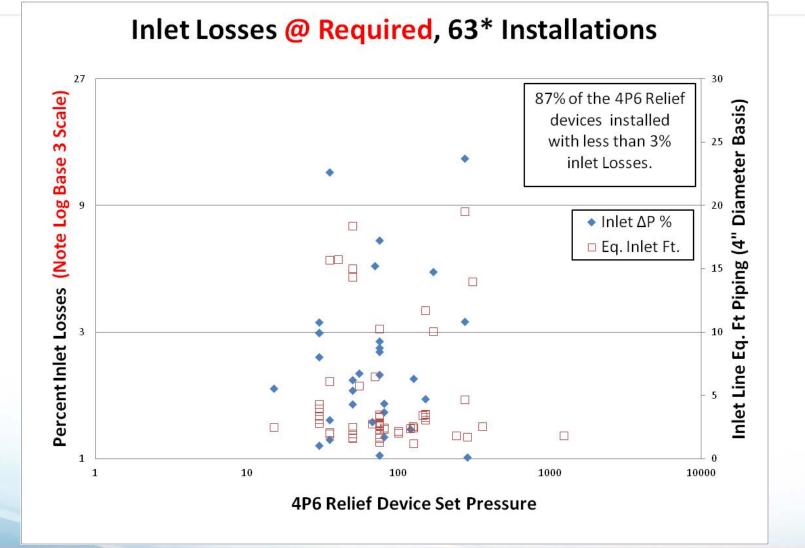
- Back to our real world problem?
- Options 4/1 do not solve any of these problems without piping modifications; arguably Option 1 will assist in the mitigation process
- Options 2/3 will reduce the number of installations that require piping modifications; let's look at the numbers:
- 48 4P6 PSVs with Inlet losses less than 3%
 - 15 were undersized so will require additional mitigation
 - 33 were acceptable
- 42 4P6 PSVs with Inlet losses greater than 3%
 - 12 were undersized so will require additional mitigation
 - 30 were adequately sized, but improperly installed
- 90 4P6 PSVs
 - 27 were undersized so will require additional mitigation
 - 63 can potentially be mitigated with PSV only changes







- Some assumptions made
- $\Delta P \propto \Delta V^2 \propto \Delta w^2 \propto (A_{Required} / A_{Orifice})^2$
- Estimated $\Delta P_{\text{Required}} \approx \Delta P_{\text{Capacity}} \times (A_{\text{Required}} / A_{\text{Orifice}})^2$
- 63 4P6 PSVs were adequately sized
 - 33 were adequately sized and Inlet Δ P less than 3%
 - 30 were adequately sized, but Inlet Δ P is greater than 3%
 - 22 have Inlet Δ P less than 3% @ the required flow rate
 - 8 have Inlet Δ P is greater than 3% @ the required flow rate
- Option 3 resolves 22 inlet Δ P cases without piping modifications
- Option 2 would resolved somewhat less than 22 cases depending on the optimized orifice size



QUESTIONS?